

Name: *A. KEY*

Question 1:

An abrupt Si BJT has the following properties at 300K:

Emitter	Base	Collector
$N_d=10^{19}\text{cm}^{-4}$	$N_a=10^{17}\text{cm}^{-3}$	$N_d=10^{15}\text{cm}^{-3}$
$\tau_p=.1\times 10^{-6}\text{s}$	$\tau_n=1\times 10^{-6}\text{s}$	$\tau_p=.1\times 10^{-6}\text{s}$
$A=10^{-4}\text{cm}^2$	$A=10^{-4}\text{cm}^2$	$A=10^{-4}\text{cm}^2$
$L_E=10\times 10^{-4}\text{cm}$	$L_B=10\times 10^{-4}\text{cm}$	$L_C=300\times 10^{-4}\text{cm}$

a) Draw the energy band diagram for the both junctions at TE.

Show

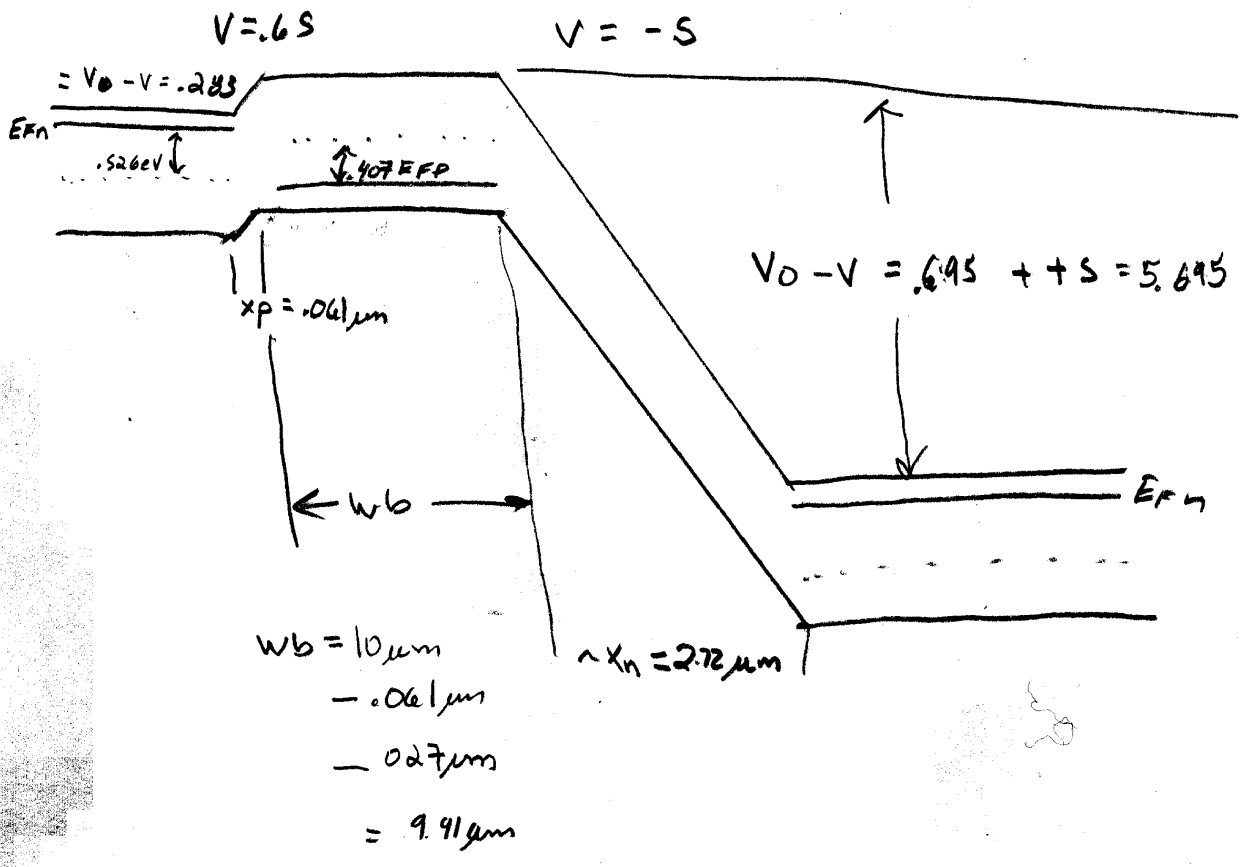
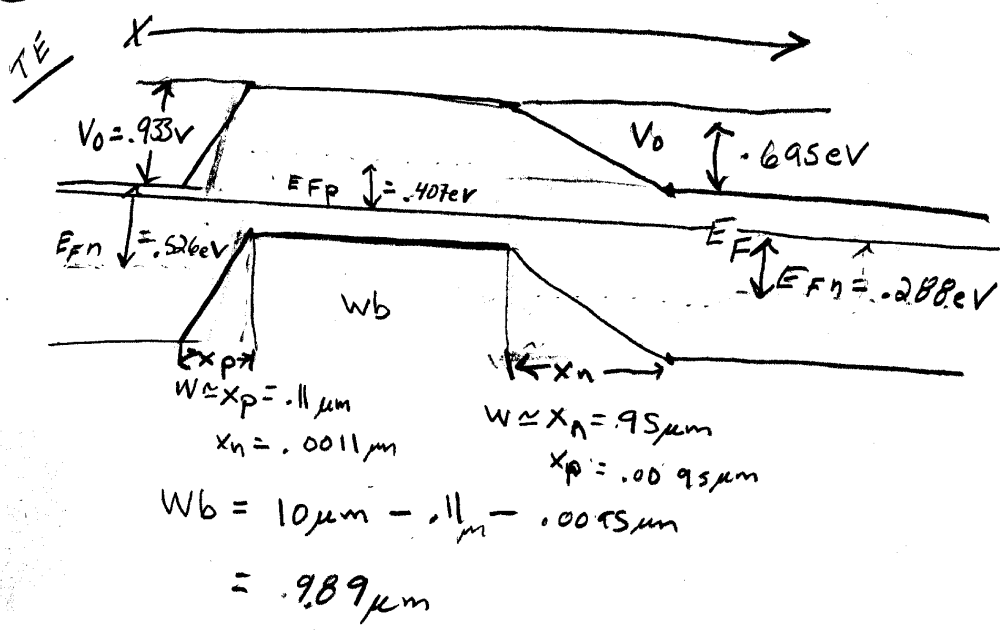
V_o for both junctions, x_n and x_p for both junctions, Fermi levels, and W_b .

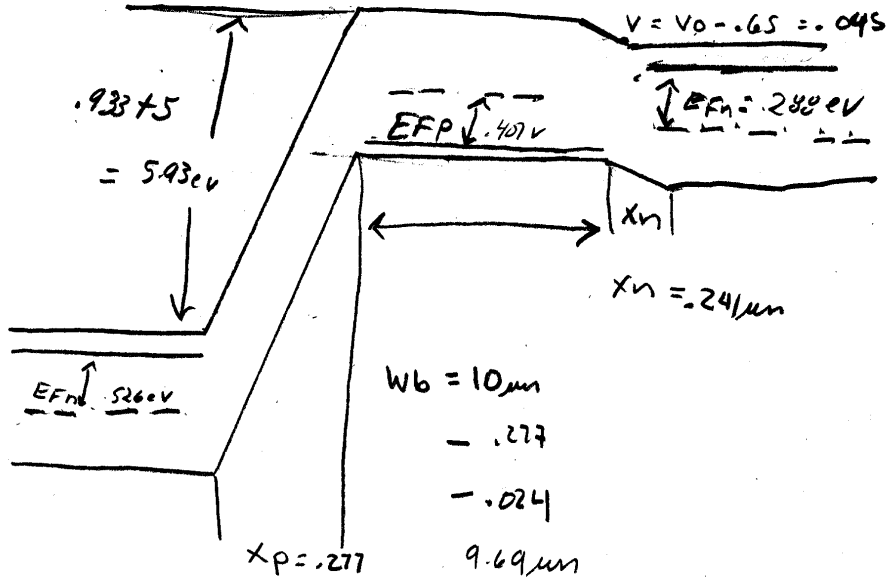
b) Draw the energy band diagram for the emitter base junction under .65 volts forward bias, and the CB junction under -5 volts reverse bias. Show V_o for both junctions, x_n and x_p for both junctions, Fermi levels, and W_b .

c) Draw the energy band diagram for the emitter base junction under -5 volts reverse bias, and the CB junction under .65 volts forward bias. Show V_o for both junctions, x_n and x_p for both junctions, Fermi levels, and W_b .

#1

1





Name: A. KEY

Question 2:

a) For the BJT in question 1 calculate emitter injection efficiency (γ), base transport factor (B), and common emitter current gain (β), under forward active and reverse active biasing.

$$W_b = 9.91 \times 10^{-4} \text{ cm} \quad V_{BE} = .65 \text{ V} \quad V_{CB} = -5 \text{ V}$$

$$W_b = 9.72 \times 10^{-4} \text{ cm} \quad V_{EB} = -5 \text{ V} \quad V_{CB} = .65 \text{ V}$$

$$\mu_n \text{ in base} = 1000 \text{ cm}^2/\text{V-s} \quad L_n = \sqrt{1000 \times 0.259 \times 1 \times 10^{-6}} = 50.89 \times 10^{-4} \text{ cm}$$

$$\mu_p \text{ in Emitter} = 100 \text{ cm}^2/\text{V-s} \quad L_{PE} = \sqrt{100 \times 0.259 \times 1 \times 10^{-6}} = 5.09 \times 10^{-4} \text{ cm}$$

$$\mu_p \text{ in collector} = 500 \text{ cm}^2/\text{V-s} \quad L_{PC} = \sqrt{500 \times 0.259 \times 1 \times 10^{-6}} = 11.3 \times 10^{-4} \text{ cm}$$

FA

$$B = 1 - \frac{1}{2} \frac{W_b^2}{L_n^2} = 1 - \frac{1}{2} \frac{9.91^2}{50.89^2} = .981$$

RA

$$B = 1 - \frac{1}{2} \frac{W_b^2}{L_n^2} = 1 - \frac{1}{2} \frac{9.72^2}{50.89^2} = .982$$

$$\gamma = \left[1 + \frac{W_b N_A \mu_{PE}}{L_{PE} N_D \mu_{nB}} \right]^{-1}$$

$$\gamma = \left[1 + \frac{W_b N_A \mu_{PC}}{L_{PC} N_D \mu_{nB}} \right]^{-1}$$

$$\gamma = .998 \quad (\text{FF})$$

$$\gamma = .0272$$

$$\alpha = \gamma B = .979$$

$$\alpha = \gamma B = .02231$$

$$\beta = \frac{\alpha}{1-\alpha} = 46.7$$

$$\beta = .0228 \text{ less than one!}$$

Name: A. KEY

Question 3:

An Si BJT has the following properties at 300K:

Emitter	Base	Collector
$N_d = 10^{19} \text{cm}^{-3}$	$N_a = 10^{17} \text{cm}^{-3}$	$N_d = 10^{19} \text{cm}^{-3}$
$\tau_p = 10 \times 10^{-6} \text{s}$	$\tau_n = 1 \times 10^{-6} \text{s}$	$\tau_p = 1 \times 10^{-6} \text{s}$
$A = 10^{-4} \text{cm}^2$	$A = 10^{-4} \text{cm}^2$	$A = 10^{-4} \text{cm}^2$
$L_E = 10 \times 10^{-4} \text{cm}$	$L_B = 10 \times 10^{-4} \text{cm}$	$L_C = 300 \times 10^{-4} \text{cm}$

- Using an excel like program, calculate W_b for the above diode with $V_{BE} = .7 \text{Volts}$ for $V_{CB} = -.5, -1, -1.5, -2, -2.5,$ and -10 volts.
- Calculate β for the above conditions.
- At what V_{CB} will W_b go to zero?
- Which is smaller the voltage you found in part c, or the breakdown voltage of the junction?

$$W_b = L_B - x_{pE} - x_{pC}$$

V_{BC}	W_b	β	γ	$\beta \alpha$
-.5	9.81 μm	.98143	.99808	47.87
-1	9.79 μm	.98151	.99806	48.08
-1.5	9.77 μm	.98158	.99808	48.27
-2	9.75	.98165	.99809	48.44
-2.5	9.73	.98171	.99809	48.59
-10	9.57	.98233	.99812	50.24

$$W_b = 10 \times 10^{-4} \text{cm} - .055 \times 10^{-4} \text{cm} - \left(\frac{2 \times 11.8 \times 8.85 \times 10^{-14}}{1.6 \times 10^{-19}} \left(V_0 - V \right) \frac{N_d}{N_a(N_d + N_a)} \right)^{1/2}$$

$$W_b = 0 \quad \angle$$

$$\left(\frac{2 \times \epsilon_s \epsilon_0}{q} \frac{V_0 - V}{N_a(N_d + N_a)} \right)^{1/2} = L_B - x_{pE}$$

$$V_0 - V = V = V_0 - \left(L_B - x_{pE} \right)^2 \frac{q N_a (N_d + N_a)}{2 N_d \epsilon_s \epsilon_0}$$

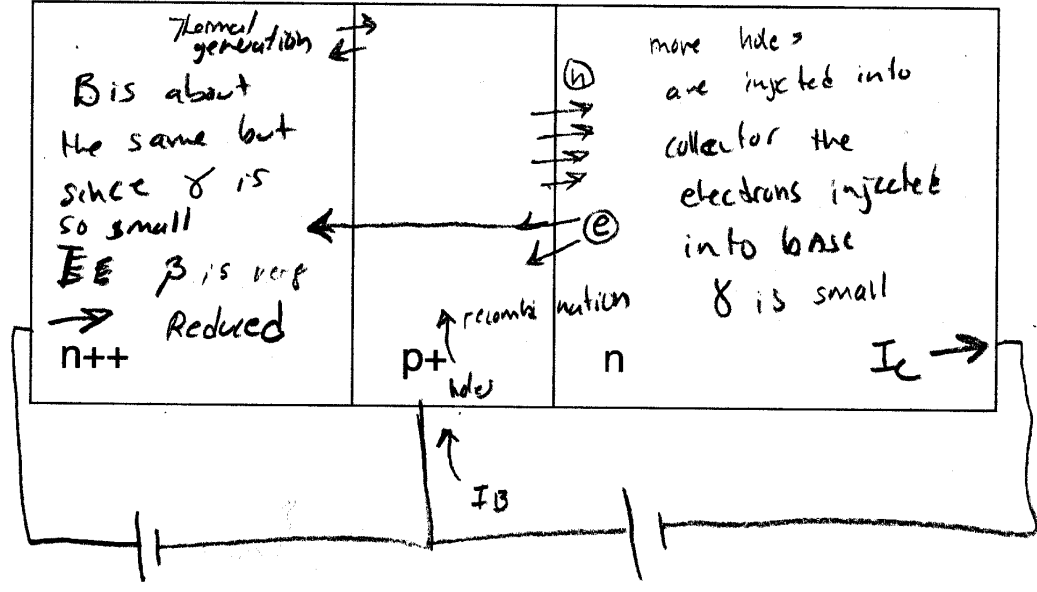
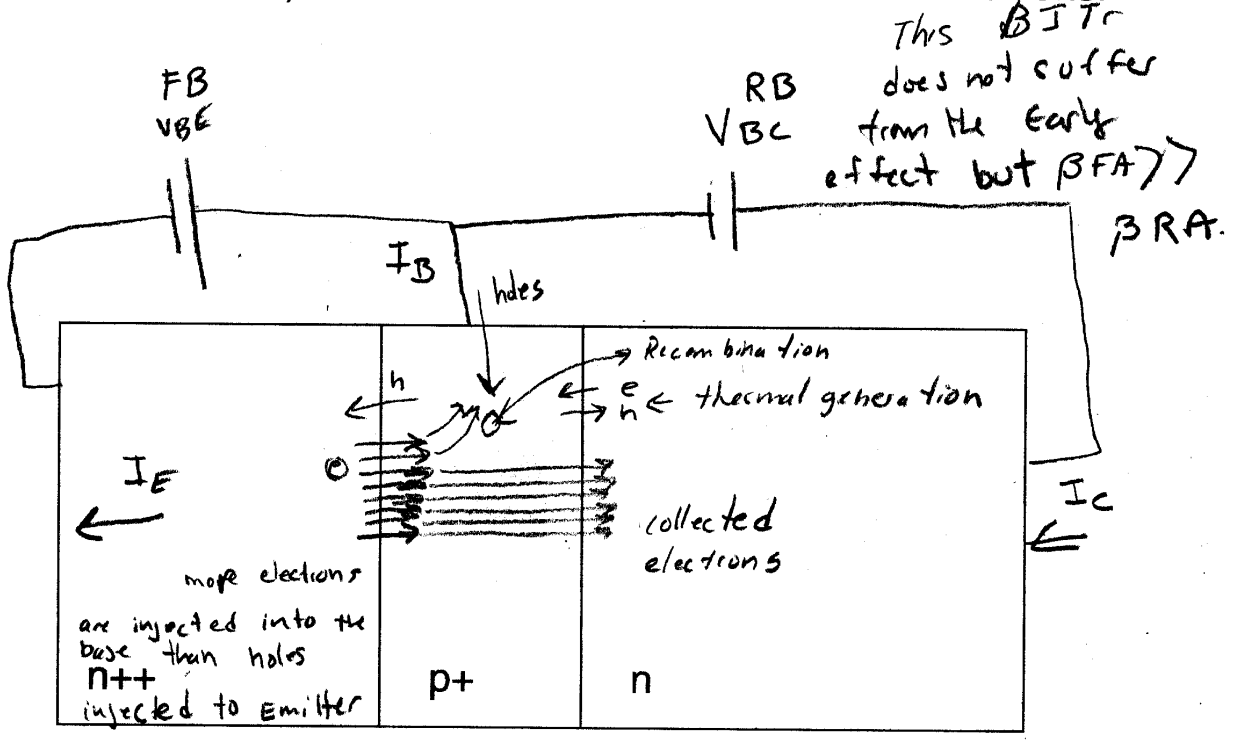
$$V = .933 - 7.622 \times 10^3 = 7621 \text{ Volts} \quad \beta \rightarrow \infty$$

d) The CB junction breaks down at about 5 volts so β will never go ∞

Name: A. KEY

Question 4:

a) Draw and label the electron and hole currents along with terminal currents. Include direction and name of current (similar to figure 7-3 in the new edition) under forward and reverse active conditions.



Question 5:

Name: A. KEY

For the diode of question 1, estimate f_T . Assume that electrons travel through the depletion region at the saturation velocity.

$$f_T = \frac{1}{2\pi\tau_d} \quad \tau_d = \tau_E + \tau_{wc} + \tau_c$$

$$\tau_E = \tau_e (C_e + C_c) \quad C_e = C_{je} + C_{se} \quad \tau_e = \frac{kT}{q I_E}$$

$$C_c = C_{jc}$$

$$I_E = qA \left(\frac{D_n n_i^2}{L_n N_A} + \frac{D_p n_i^2}{L_p N_D} \right) \left(e^{\frac{V_f}{kT}} - 1 \right)$$

\uparrow $W_b!$

$$I_E = 1.6 \times 10^{-19} \times 10^{-4} \left(\frac{0.0259 \times 1000 \times 1.5 \times 10^{10}}{9.9 \times 10^{-4} \times 1 \times 10^{17}} \right) e^{\frac{0.65}{0.0259}} = 5.88 \times 10^{-6} \text{ C}$$

$$= 46 \times 10^{-6} \text{ Amps}$$

$$C_{se} = \frac{q}{kT} I_E \tau_E = \frac{1}{0.0259} \times 46 \times 10^{-6} \times 1 \times 10^{-6} = 1.8 \text{ nF}$$

$$C_{je} = \frac{A}{2} \left[\frac{2qE}{V_0 - V} N_A \right]^{1/2} = \frac{10^{-4}}{2} \left[\frac{2 \times 1.6 \times 10^{-19} \times 11.8 \times 8.85 \times 10^{-14} \times 1 \times 10^{17}}{0.935 - 0.65} \right]^{1/2}$$

$$= 17 \text{ pF}$$

$$C_{jc} = \frac{A}{2} \left[\frac{2qE}{V_0 - V} N_D \right]^{1/2} = \frac{10^{-4}}{2} \left[\frac{2 \times 1.6 \times 10^{-19} \times 11.8 \times 8.85 \times 10^{-14} \times 1 \times 10^{15}}{0.935 + 0.65} \right]^{1/2}$$

$$= 0.38 \text{ pF}$$

$$\tau_E = \frac{0.0259}{46 \times 10^{-6}} [1.8 \text{ nF} + 17 \text{ pF} + 0.38 \text{ pF}] = 1.02 \times 10^{-6} \text{ seconds}$$

Note: $\tau_E \approx \tau_n \times 10^{-6} s$! If we want to switch faster we have to decrease τ_n which lowers the gain.

$$\tau_{WC} = \frac{W_{CB} \overset{\text{depletion width}}{\approx} x_n}{2 \langle v_{sat} \rangle} = \frac{2.72 \times 10^{-4} \text{ cm}}{2 \times 10^{17} \frac{\text{cm}}{\text{s}}} = 13 \text{ ps}$$

$$\tau_t = \frac{W_D^2}{2 D_n} = \frac{9.91 \times 10^{-4} \text{ cm}^2}{2 \times 1000 \text{ cm}^2/\text{V}\cdot\text{s} \times 0.025 \text{ V}} = 18 \text{ ns}$$

$$\tau_d = 1.02 \times 10^{-6} \text{ s} + 13 \text{ ps} + 18 \text{ ns}$$

$$\tau_d = 1.038 \times 10^{-6}$$

$$f_T = \frac{1}{2\pi \times 1.038 \times 10^{-6}} = 153 \text{ MHz}$$

What if we changed τ_n to $1 \times 10^{-9} \text{ s}$?

$$\tau_d \approx 1 \times 10^{-9} \text{ s} + 13 \text{ ps} + 18 \text{ ns} = 19 \text{ ns}$$

$$f_T = 8.37 \text{ MHz}$$

If we switched to a graded base $\tau_t = \frac{W_B^2}{4 D_n}$

$$f_T = 15.89 \text{ MHz}$$

If we $\frac{1}{2} W_B$ (no graded base) $\tau_t = \frac{\left(\frac{W_B}{2}\right)^2}{2 D_n} = \frac{W_B^2}{8 D_n} = 4.8 \text{ ns}$
 $f_T = 27 \text{ MHz}$ $\frac{W_B}{10} \rightarrow f_T \rightarrow 133 \text{ MHz}$

Question 6:

Name: A. KEY

For an npn BJT, How do you scale W_b to keep the same common emitter current gain (β) if you decrease τ_n by a factor of 10?

Assume since $W_b \ll L_n$ emitter injection efficiency is not affected by changes in W_b , so that

leaves us
$$\beta = 1 - \frac{1}{2} \frac{W_b^2}{(\sqrt{D_n \tau_n})^2}$$

$$1 - \frac{1}{2} \frac{W_{b \text{ old}}^2}{(\sqrt{D_n \tau_{n \text{ old}}})^2} = 1 - \frac{1}{2} \frac{W_{b \text{ new}}^2}{\left(\sqrt{D_n \frac{\tau_{n \text{ old}}}{10}}\right)^2}$$

$$\frac{W_{b \text{ old}}^2}{\tau_{n \text{ old}}} = \frac{W_{b \text{ new}}^2}{\frac{\tau_{n \text{ old}}}{10}}$$

$$W_{b \text{ new}}^2 = \frac{W_{b \text{ old}}^2}{10}$$

$$W_{b \text{ new}} = \frac{W_{b \text{ old}} \sqrt{10}}{\sqrt{10}}$$

Name: A. KEY

Question 7:

List and explain some methods of increasing the switching speed of BJTs. Include the engineering tradeoffs you have to make.

$$f_T = \frac{1}{2\pi \tau_d} \quad f_{MAX} = \left(\frac{f_T}{2\pi R_B C_c} \right)^{1/2}$$

$$\tau_E = \frac{kT}{qI} \left(\frac{qI\tau_D}{kT} + C_c + C_e \right) \approx \tau_n$$

If we minimize τ_n then β goes down $\beta = 1 - \frac{w_b^2}{2\tau_n v_{on}}$

If we scale down w_b τ_E goes down as well

$\frac{w_b^2}{2\tau_n}$ and the gain can be brought back up.

however R_B increases a w_b decreases and f_{MAX} will go down.

C_c is C_{jc} and the larger the V_{BC} the smaller

C_{jc} is, but $\tau_{we} = \frac{w_{cB}}{v_{sat}}$ will increase right? v_{sat}

$$C_{jc} = \frac{A \epsilon_{si}}{w_{cB}}$$